(19) Europäisches Patentamt
European Patent Office
Office européen des brevets

(11) EP 2 551 522 B1

(12) **EUROPEAN PATENT SPECIFICATION**

(45) Date of publication and mention of the grant of the patent:
23.10.2019 Bulletin 2019/43

(51) Int Cl.:
F04B 35/04 *(2006.01)* ***F04B 49/06*** *(2006.01)*
F04B 17/04 *(2006.01)*

(21) Application number: **12178264.3**

(22) Date of filing: **27.07.2012**

(54) **HIGH PRESSURE SOLENOID PUMP**

HOCHDRUCKSOLENOIDPUMPE

POMPE À SOLÉNOÏDE À HAUTE PRESSION

(84) Designated Contracting States:
AL AT BE BG CH CY CZ DE DK EE ES FI FR GB GR HR HU IE IS IT LI LT LU LV MC MK MT NL NO PL PT RO RS SE SI SK SM TR

(30) Priority: **28.07.2011 US 201113192824**

(43) Date of publication of application:
30.01.2013 Bulletin 2013/05

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Printed by Jouve, 75001 PARIS (FR)

Description

[0001] The invention relates generally to a solenoid pump with a conical, variable rate spring to enable maximum displacement of a plunger in the pump and to increase back pressure values under which the pump can operate. The invention also generally relates to a control scheme for a solenoid pump that varies a duty cycle according an input voltage used to power the pump.

[0002] The Japanese Patent Application JP 2009 047035 A discloses a control device of the electromagnetic fuel pump. The control device is used for forcibly feeding fuel toward the combustion equipment by reciprocatively operating a member for constituting a part of a fuel pressurizing chamber by a variation in magnetic force by periodic current-carrying to an electromagnetic coil. The control device executes control in the direction for adapting a pump delivery flow rate by following a variation in a request fuel flow rate of the combustion equipment by changing a width of a delivery stroke.

[0003] The US-Patent US 4,496,287 A shows a sensor which provides information about the fluid itself, such as its quality as measured by its density or viscosity, or about the state of a fluid system which contains it, such as the fluid pressure existing at some point in the system. The sensor includes a fluid displacement device or element physically adapted to displace the fluid and repetitively urged into displacement by the application of a known impetus or urging force. The resulting motion of the element is then analyzed to obtain the information desired. Springs are used to assist the displacement.

[0004] The international patent application WO 03/023226 A1 discloses an electronic control systems and process for infusion devices and pump configurations. The system includes a capacitor, which is controlled to partially, but not fully discharge, to provide a power pulse to a pump coil. A power cut-off switch is be provided to control the discharge of the capacitor such that the capacitor is stopped from discharging prior to the actual end of the armature stroke.

[0005] The Japanese Patent Application JP 2010 065611 A provides a fluid injection device. The fluid injection device includes a fluid chamber changing a fluid injection part having a connecting flow passage communicating one end part with an outlet flow passage and arranging a fluid injection opening part in the other end part. A connecting flow passage pipe is used for transmitting pulsation to the fluid injection opening part. A pump supplies fluid. A driving part supplies a driving signal to a piezoelectric element.

[0006] Known solenoid pumps use linear springs to bias a plunger against displacement by a solenoid coil in a pumping cycle. When the springs are fully compressed, the springs occupy an undesirably large space since the coils for the springs stack upon each other. Known control schemes for solenoid pumps use a fixed duty cycle, typically 50, regardless of the magnitude of the input voltage to be used to energize the solenoid coils for the pumps. As a result, too little power is delivered to the coils for low values of the input voltage and the coils remain energized even after plungers for the pumps have fully displaced to fully compress the springs for the pumps. As a result, the pumps consume unnecessarily high amounts of energy and undesirable amounts of heat are generated, which degrades operation of the pumps.

[0007] Typically, back pressure is present at the outlet port of a solenoid pump and limits operation of the pump, that is, the pump can operate only up to a certain back pressure level. In general, the back pressure works against the spring used to bias the plunger. For example, when the back pressure is greater than the biasing force of the spring, the pumping cycle is terminated (the plunger cannot return to a "rest" position when the coil is de-energized). The known use of linear springs limits the back pressure under which known solenoid pumps can operate. The spring biasing force must be relatively lower to enable the initiation of the plunger displacement when the coil is energized. Since the spring is linear, only the same relatively lower biasing force is available to counteract the back pressure. Known solenoid pumps cannot operate with a backpressure over about 10 psi.

[0008] Common rail systems use a relatively low pressure pump to pump fuel from a fuel source to a high pressure pump. The high pressure pump supplies fuel from the low pressure pump to a distribution line, for example, a distribution pipe feeding fuel injectors for an engine. The high pressure pump in a common rail system can operate at pressures of over 29,000 psi. A pressure regulating valve placed between the low and high pressure pumps typically creates a back pressure on the outlet port of the low pressure pump greater than the 10 psi maximum backpressure under which known solenoid pumps can operate. Thus, known common rail systems teach the use of pumps other than solenoid pumps.

[0009] According to aspects illustrated herein, there is provided a control unit for a solenoid pump including: an inlet port, an outlet port, and a first through-bore connecting the inlet and outlet ports; a plunger disposed within the first through-bore and including a second through-bore; a spring arranged to urge the plunger toward the outlet port; a solenoid coil disposed about a portion of the plunger and arranged to displace the plunger toward the inlet port in response to coil power applied to the solenoid coil, the control unit including: an input for accepting an input voltage; and a power circuit for: generating the coil power during an interval equal to a time period; supplying the coil power to the solenoid coil; and selecting a duration of the time period such that the duration of the time period varies according to the input voltage.

[0010] According to aspects illustrated herein, there is provided a solenoid pump, including: an inlet port, an outlet port, and a first through-bore connecting the inlet and outlet ports; a plunger disposed within the first through-bore and including a second through-bore; a spring arranged to urge the plunger toward the outlet port; a solenoid coil disposed about a portion of the plunger and arranged to displace the plunger toward the inlet port in response to coil power applied to the solenoid coil; and a control unit for: accepting an input voltage; generating the coil power during an interval equal to a first time period; supplying the coil power to the solenoid coil; and selecting a duration of the first time period such that the duration of the first time period varies according to the input voltage.

[0011] According to aspects illustrated herein, there is provided a solenoid pump, including: a housing with an inlet port and an outlet port; a first through-bore connecting the inlet and outlet ports; a plunger disposed within the first through-bore and including a second through-bore; a spring arranged to urge the plunger toward the outlet port; a solenoid coil arranged to displace the plunger toward the inlet port in response to a coil power applied to the solenoid coil; and a control unit for controlling operation of the solenoid coil such that when the solenoid coil is energized by the coil power to displace the plunger and the spring is fully compressed by the plunger, coils forming the spring are aligned in a direction orthogonal to a longitudinal axis passing through the inlet and outlet ports.

[0012] According to aspects illustrated herein, there is provided a solenoid pump, including: a housing with an inlet port and an outlet port; a first through-bore connecting the inlet and outlet ports; a sleeve disposed within the first through-bore and displaceable parallel to a longitudinal axis passing through the inlet and outlet ports; a plunger disposed within the first through-bore, displaceable parallel to the longitudinal axis, and including a second through-bore; a spring arranged to urge the plunger toward the outlet port; a solenoid coil arranged to displace the plunger toward the inlet port in response to a coil power applied to the solenoid coil; and a control unit for controlling operation of the solenoid coil such that fluid is transferred from the inlet port to the outlet port through the second through bore.

[0013] According to aspects illustrated herein, there is provided a method of operating a control unit for a solenoid pump including: an inlet port, an outlet port, and a first through-bore connecting the inlet and outlet ports; a plunger disposed within the first through-bore and including a second through-bore; a spring arranged to urge the plunger toward the outlet port; a solenoid coil disposed about a portion of the plunger and arranged to displace the plunger toward the inlet port in response to coil power applied to the solenoid coil, the method including: using an input to accept an input voltage; and using a power circuit to: generate the coil power during an interval equal to a time period; supply the coil power to the solenoid coil; and select a duration of the time period such that the duration of the time period varies according to the input voltage.

[0014] According to aspects illustrated herein, there is provided a method of pumping fluid using a solenoid pump including: an inlet port, an outlet port, and a first through-bore connecting the inlet and outlet ports; a plunger disposed within the first through-bore and including a second through-bore; a spring; a solenoid coil disposed about a portion of the valve assembly; and a control unit. The method includes: urging, using the spring, the plunger toward the outlet port; and using the control unit to: accept an input voltage; determine a magnitude of the input voltage; select a duration of a first time period such that the duration of the first time period varies according to the input voltage; generating, using the input voltage, a coil power during an interval equal to the first time period; supplying the coil power to the solenoid coil such that the plunger displaces toward the inlet port; remove the coil power such that the spring displaces the plunger toward the outlet port.

[0015] According to aspects illustrated herein, there is provided a method of pumping fluid using a solenoid pump including: a housing with an inlet port and an outlet port; a first through-bore connecting the inlet and outlet ports; a plunger disposed within the first through-bore and including a second through-bore; a spring; a solenoid coil; and a control unit. The method including: urging the plunger toward the outlet port with the spring; and using the control unit to apply a coil power to the solenoid coil to displace the plunger toward the inlet port such that the spring is fully compressed by the plunger, and coils forming the spring are aligned in a direction orthogonal to a longitudinal axis passing through the inlet and outlet ports.

[0016] The nature and mode of operation of the present invention will now be more fully described in the following detailed description of the invention taken with the accompanying drawing figures, in which:

Figure 1 is a plan view of a high pressure solenoid pump;

Figure 2 is a side view of the pump shown in Figure 1;

Figure 3 is an exploded view of the high pressure solenoid pump shown in Figure 1;

Figures 4A - 4C are respective cross-sectional views of the high pressure solenoid pump shown in Figure 1 generally along line 4-4 in Figure 1, depicting various stages of a pumping cycle;

Figure 5A is a table showing duty cycle data for a solenoid pump using a control scheme varying a time for generating coil power;

Figure 5B is a table for a prior art control scheme with a fixed duty cycle;

Figure 6 depicts an exemplary power circuit for a control scheme varying a time for generating coil power according to input voltage.

[0017] At the outset, it should be appreciated that like drawing numbers on different drawing views identify identical, or functionally similar, structural elements of the invention. It is to be understood that the invention as claimed is not limited to the disclosed aspects.

[0018] Furthermore, it is understood that this invention is not limited to the particular methodology, materials and modifications described and as such may, of course, vary. It is also understood that the terminology used herein is for the purpose of describing particular aspects only, and is not intended to limit the scope of the present invention, which is limited only by the appended claims.

[0019] Unless defined otherwise, all technical and scientific terms used herein have the same meaning as commonly understood to one of ordinary skill in the art to which this invention belongs. Although any methods, devices or materials similar or equivalent to those described herein can be used in the practice or testing of the invention, exemplary methods, devices, and materials are now described.

[0020] Figure 1 is a plan view of high pressure solenoid pump 100.

[0021] Figure 2 is a side view of pump 100 shown in Figure 1.

[0022] Figure 3 is an exploded view of high pressure solenoid pump 100 shown in Figure 1.

[0023] Figures 4A - 4C are respective cross-sectional views of high pressure solenoid pump **100** shown in Figure 1 generally along line 4-4 in Figure 1, depicting various stages of a pumping cycle. The following should be viewed in light of Figures 1 through 4C. Pump **100** includes housing **102** with inlet port **104** and outlet port **106.** In an example embodiment, housing **102** is formed by main housing **102A,** inlet housing **102B,** and outlet housing **102C.** Housings **102B** and **102C** are connected to the main housing by any means known in the art, for example, threads. Pump **100** includes through-bore **108** connecting the inlet and outlet ports **104** and **106,** and plunger **110** disposed within through-bore **108** and including through-bore **112.** Pump **100** includes spring **114** arranged to urge the plunger **110** toward the outlet port **106,** solenoid coil **116** arranged to displace the plunger **110** toward the inlet port **104** in response to a coil power applied to the solenoid coil **116,** and control unit **118** for controlling operation of the solenoid coil **116.**

[0024] Spring **114** is a variable rate spring. By "variable rate spring" we mean that resistance of the spring to compression of the spring **114** in direction **A1** toward the inlet port **104** increases as the spring is compressed in direction **A1,** for example, by the plunger. Stated otherwise, referring to Hooke's Law: F = -kx, the constant k for the spring **114** increases as the spring **114** is compressed. Thus, the further the spring **114** is compressed, the more force is needed to continuing compressing the spring **114.** For example, when the plunger **110** begins displacing in direction **A1** from the position shown in Figure 4A, a certain amount of force is required to compress the spring **114**. As the plunger **110** continues to displace to the position shown in Figure 4B, an increasingly greater amount of force is required to continue compressing the spring **114**. The rate for spring **114** may vary according to pump type and the pressure output of the pump **100**, for example, k for the spring **114** can be varied.

[0025] Spring **114** has a conical shape, for example, diameter **D1** at end **120** of the spring **114** closest to the inlet port **104** in Figure 4A is less than diameter **D2** at end **122** of the spring **114**, opposite end **120**. Thus, when the spring **114** is compressed as shown in Figure 4B, compressed coils **124** forming the spring **114** are aligned in direction **R** orthogonal to longitudinal axis **126** passing through the inlet and outlet ports **104** and **106**.

[0026] In an example embodiment, the pump **100** includes a sleeve **128** disposed within through-bore **108** and displaceable parallel to axis **126**. The plunger **110** is disposed within the sleeve **128** and in an example embodiment is displaceable within the sleeve **128** parallel to the longitudinal axis **126**. Seals **130**, for example, O-rings, provide a seal between housing **102** and the sleeve **128**, while enabling movement of the sleeve **128** within bore **108**. Length **L1** of the sleeve **128** is less than length **L2** of through bore **108**, thus, the sleeve **128** "floats" within bore **108**. Advantageously, having sleeve **128** "float" within bore **108** increases the ease of fabrication of pump **100**, since fabrication steps that would be needed to fix the sleeve **128** within the pump **100** are eliminated. Further, having the sleeve **128** float enables greater flexibility since sleeves **128** with different lengths **L1** can be easily installed. Also, since **L1** is less than **L2**, tolerances for **L1** can be relaxed, reducing manufacturing cost and complexity. In an example embodiment, sleeve **128** is made from a non-magnetic material.

[0027] The following provides further example detail regarding pump **100** and an example operation of pump **100.** The plunger **110** is arranged to pass fluid through through-bore **112** and longitudinally traverses the pump **100** between the inlet and outlet ports **104** and **106.** In an example embodiment, bumper spring **132** is disposed in end **134** of the plunger **100.** The bumper spring **132** contacts shoulder **136** in the housing **102** to cushion the impact of the plunger **110** as the plunger **110** moves from the position of Figure 4B to the fully retracted position of Figure 4A. Sleeve **128** serves as the primary location wherein mechanical pumping operations are performed. Suction valve assembly **138** is disposed at end **140** of the plunger **110.** In an example embodiment, the suction valve assembly **138** includes cap **142,** seat **144,** and stem **146** passing through retainer element **148.** The operation of the suction valve assembly **138** is further described below.

[0028] Pump **100** includes one-way check valve **150.** The check valve **150** enables fluid flow through the inlet port **104** toward the outlet port **106** in direction **A2** and blocks fluid flow in the opposite direction, **A1**. In an example embodiment, the check valve **150** includes sealing element **152** within valve housing **154**. The sealing element **152** seals against the housing **102**, for example, inlet housing **102B** to block flow out of the pump **100** through the inlet port **104**. For example, the one-way check valve **150** is used as part of drawing fuel from a fuel source such as a fuel tank.

[0029] Figure 4A shows plunger **110**, the suction valve assembly **138**, the check valve **150**, and spring **114** in respective rest positions. While coil **116** is not energized, spring **114** biases, or urges, plunger **110** in direction **A2** such that the bumper spring is in contact with shoulder **136**. If backpressure exists, i.e., pressure caused by fluid entering from outlet port **106**, cap **142** forms a seal with seat **144** to prevent fluid from flowing from bore **112** past the suction valve assembly **138** in direction **A1.** The seal in the check valve **150** prevents fluid flowing from flowing past the check valve **150** and out through the inlet port **104**.

[0030] Figure 4B illustrates coil 116 as being energized, which forms a magnetic field. The magnetic field created by the energized coil imparts a directional force upon plunger 110 in direction A1 toward inlet port 104, causing the plunger 110 to displace in direction **A1** and spring **114** to compress. As a result of the movement in direction **A1** and the configuration of the suction valve assembly **138**, a negative pressure, or suction, is formed in chamber **158** of through-bore **108** and through-bore **112**, displacing cap **142** from seat **144**. Fluid present in chamber **156** in through-bore **108** just prior to energizing coil **116** is sucked around the suction valve assembly **138**, as shown by flow lines **F1,** and into chamber **158** in through-bore **112**. During this stage, fluid is prevented from moving between chamber **156** and inlet port **102** by the check valve **150**.

[0031] Referring now to Figure 4C, as coil **116** is de-energized, the magnetic field collapses. As a result, plunger **110** is no longer acted upon by a magnetic force and is urged in direction **A2** toward to the rest location of Figure 4A by the bias of spring **114.** Two simultaneous events occur during the movement of plunger **110** in direction **A2.** First, fluid contained in bore **112** and chamber **158** is forced out of outlet port **104,** as shown by fluid flow lines **F2.** The fluid in bore **112** and chamber **158** is prevented from entering chamber **156** by the seal created between cap **142** and seat **144.** Simultaneously, fluid is replenished in chamber **156** as follows. As plunger **110** moves in direction **A2**, a negative pressure, or suction, is created in chamber **156.** The negative pressure causes the check valve **150** to open, allowing fluid to be drawn from inlet port **102** into chamber **156**, as shown by fluid flow lines **F3.**

[0032] The operation described above regarding Figures 4A through 4C is cyclically repeated during the use of the pump **100.** As described below, the control unit **118** energizes the solenoid coil **116** for a particular time period $\mathbf{T_{off}}$, and de-energizes the solenoid coil **116** for a particular time period $\mathbf{T_{on}}$ for example, while generating the power to operate the solenoid coil **116**. This means that during each cycle of operation, the plunger **110** is biased in direction **A1** by electromagnetic force for $\mathbf{T_{off}}$, and then biased in direction **A2** by spring **114** for the particular time period $\mathbf{T_{on}}$. The reciprocal motion causes fluid to flow through inlet port **102** and the check valve **150** into chamber **156**, through the suction valve assembly into chamber **158**, and through outlet port **106**, thereby creating a continuous flow of fluid.

[0033] As noted above, some amount of back pressure, that is, pressure exerted through the outlet port **106** into through-bore **108** in direction **A1**, is typically present during operation of pump **100**. The back pressure biases the plunger **110** in direction **A1**, against the biasing of spring **114**. When the force of the back pressure is greater than the force exerted by spring **114**, for example, spring **114** no longer can urge the plunger **110** in direction **A2** from the position in Fig. 4B, the reciprocating action of the plunger **110** is terminated and fluid no longer can be transferred as described above. Known solenoid pumps using nominal 12VDC input power cannot operate (pump fluid) above about 10 psi of back pressure.

[0034] Advantageously, pump **100** is able to operate (pump fluid) up to about 15 psi of back pressure. The ability of pump **100** to operate at greater back pressures is at least partly due to the variable rate of spring **114.** Due to the characteristics associated with operation of the solenoid coil **116**, it is desirable to minimize the amount of resistance the plunger **110** must overcome at the onset of a cycle. As noted above, the variable rate results in spring **114** advantageously generating relatively less biasing force resisting movement of the plunger **110** in direction **A1** at the onset of a pump cycle, for example, starting in the position of Figure 4A. Also as noted above, the biasing force of spring **114** increases as the spring **114** is compressed, such that in the position shown in Figure 4B, the biasing force is maximized. This maximized force initiates the movement of the plunger **110** in direction **A2** after the solenoid coil **116** is de-energized. Advantageously, the biasing force generated by spring **114** when the solenoid coil **116** is de-energized determines the amount of back pressure under which pump **100** can operate. That is, the greatest amount of biasing force from spring **114** is needed to initiate displacement of the plunger **110** against the back pressure when the solenoid coil **116** is de-energized. Thus, spring **114** provides the least resistance when less resistance is advantageous, that is, when the solenoid coil **116** is first energized and the displacement of the plunger **110** in direction **A1** begins; and provides the most resistance when more resistance is advantageous, that is, when the solenoid coil **116** is de-energized and spring **114** must operate against the back pressure.

[0035] Pump **100** can be used in common rail systems. As noted above, in a common rail system a relatively low pressure pump is used to pump fuel from a fuel source to a high pressure pump. For a common rail system, the back pressure on the outlet port of the low pressure pump is greater than the 10 psi maximum backpressure under which known solenoid pumps can operate. Advantageously, the approximately 15 psi maximum backpressure under which pump **100** can operate is sufficient to enable operation of pump **100** in a common rail system.

[0036] Figure 5A is a table showing duty cycle data for a solenoid pump using a control scheme varying a time for generating coil power **CP.**

[0037] Figure 5B is a table for a prior art control scheme with a fixed duty cycle. By duty cycle for a pump, we mean the percentage of the cycle during which the coil power is generated using the input voltage **IV.** Pump **100** is referenced in the discussion that follows; however, it should be understood that the control scheme described below is applicable to any solenoid pump using a solenoid coil **116** to displace an element to transfer fluid from an inlet port **104** for the pump **100** to an outlet port **106** for the pump **100.** Control unit **118** is for controlling operation of the solenoid coil **116.** The control unit **118** is for accepting input voltage **IV**, for example, from an outside source, such as a battery of a vehicle in which the pump **100** is installed. It should be understood that any source of voltage known in the art can be used to provide input voltage **IV.**

[0038] The control unit **118** makes a determination regarding a magnitude of the input voltage **IV** and generates the coil power **CP** during an interval equal to a time period $\mathbf{T_{off}}$. That is, the interval is the time period $\mathbf{T_{off}}$ used by the control unit **118** to generate the coil power **CP.** The control unit **118** supplies the coil power to the solenoid coil . The control unit selects a duration of the time period $\mathbf{T_{off}}$ such that the duration of the time period $\mathbf{T_{off}}$ varies according to the determination of the magnitude of the input voltage. That is, the duration of the time period $\mathbf{T_{off}}$ is proportional to the magnitude of **IV.** The combination of the magnitude **of IV** and the duration of the time period $\mathbf{T_{off}}$ determine the magnitude of the coil power **CP** as further described *infra.*

[0039] The following should be viewed in light of Figures 4A through 5B. A cycle for pump **100** is defined as the time required for the pump **100** to operate such that the plunger **110** begins at the position shown in Figure 4A and returns to the position shown in Figure 4C. That is, a cycle is a cycle of operation for the plunger **110**, spring **114**, and the pump **100** to transfer a fluid from the inlet port **104** to the outlet port **106.** At the start of the cycle, the solenoid coil **116** is de-energized by the control unit **118** such that the plunger **110** is in the position, within through-bore **108** and proximate the outlet port **106**, shown in Figure 4A. To complete the cycle: the control unit **118** energizes the solenoid coil **116** by applying the coil power for time period $\mathbf{T_{off}}$ such that the plunger **110** is displaced to the position, within sleeve **128** and proximate the inlet port **104**, shown in Figure 4B; and the control unit **118**de-energizes the solenoid coil **116** by removing the coil power such that the plunger **110** moves to the position in Figure 4C and then to the position shown in Figure 4A.

[0040] Advantageously, the control unit **118** is for decreasing the duration of the time period $\mathbf{T_{off}}$ as the magnitude of the input voltage **IV** increases; and increasing the duration of $\mathbf{T_{off}}$ as the magnitude of the input voltage **IV** decreases. In an example embodiment, the control unit **118** compares the input voltage **IV** to a pre-determined value. If the input voltage **IV** is greater than the value, the control unit **118** decreases the time period $\mathbf{T_{off}}$ in proportion to the difference between the input voltage **IV** and the value, with the time period $\mathbf{T_{off}}$ decreasing as the difference increases. If the input voltage **IV** is less than the value, the control unit **118** increases the time period $\mathbf{T_{off}}$ in proportion to the difference between the input voltage **IV** and the value, with the time period $\mathbf{T_{off}}$ increasing as the difference increases. Figure 5A shows an exemplary variation of the time period $\mathbf{T_{off}}$ with respect the variation of the input voltage **IV.** In an example embodiment, a minimum time period is necessary for the plunger **110** to fully displace from the position shown in Figure 4A to the position shown in Figure 4B, and the control unit **118** ensures that $\mathbf{T_{off}}$ is greater than the minimum time period $\mathbf{T_{off}}$.

[0041] As noted above, the control unit is for supplying the coil power to the solenoid coil **116** during time period $\mathbf{T_{off}}$. For an input voltage **IV** greater than a pre-determined value, the control unit **118** is for selecting the duration of $\mathbf{T_{off}}$ to be less than the duration of $\mathbf{T_{on}}$. For an input voltage **IV** less than the pre-determined value, the control unit **118** is for selecting the duration of the time period $\mathbf{T_{off}}$ to be greater than the duration of $\mathbf{T_{on}}$. In an example embodiment, $\mathbf{T_{on}}$ is constant regardless of $\mathbf{T_{off}}$.

[0042] As noted above, a duty cycle for a pump **100** is defined as the percentage of the cycle during which the coil power is generated using the input voltage **IV.** For example, for a control scheme charging a capacitor with the input voltage **IV** to generate the coil power, the duty cycle is the percentage of the cycle during which the capacitor is charged. For the control scheme depicted in Figure 5A and described above, the duty cycle advantageously varies according to the magnitude of the input voltage. For example, in Figure 5A, the duty cycle decreases with increasing the input voltage **IV.** In contrast, as shown in Figure 5B, the duty cycle is constant regardless of the value of the input voltage **IV**, with attendant disadvantages and problems as described below.

[0043] In an example embodiment, the input voltage **IV** is a direct current voltage and **CP** is an alternating current voltage. The control unit **118** is for: supplying the coil power at a specific frequency; and selecting a magnitude of the frequency such that the magnitude of the frequency varies according to the magnitude of the input voltage **IV.** Thus, the control unit **118** decreases the magnitude of the frequency as the magnitude of the input voltage decreases, and increases the magnitude of the frequency as the magnitude of the input voltage **IV** increases as shown in Figure 4A.

[0044] As shown in Figure 5B, and noted *supra,* known control schemes do not vary $\mathbf{T_{off}}$ or **CP** to account for changes in the input voltage **IV**, that is, the duty cycle is constant. For example, in Figure 5B, $\mathbf{T_{off}}$ is 23 milliseconds (ms) regardless of the value for the input voltage

IV. As a result, a less than desirable amount of power is delivered to the solenoid coil **116** for lower values of the input voltage **IV**, for example, 10V in Figure 5B, resulting in incomplete displacement of the plunger **110** by the solenoid and an undesirable decrease in pumping capacity for the pump **100.** As the value of the input voltage **IV** increases with the known control schemes, a different problem arises. At higher values of **IV**, for example, 14V in Figure 5B, the plunger **110** is fully extended for a relatively long period before the expiration of $\mathbf{T_{off}}$. As a result, the solenoid coil **116** continues to be energized even though the plunger **110** is fully extended, which leads to undesirable overheating of components in the pump **100**, such as control circuitry. For example, electronic components in the circuitry, such as transistors, can overheat due to the preceding conditions. Further, the power efficiency of the pump **100** is decreased since excessive amounts of power are consumed by components in the pump **100**, such as the control circuitry, without producing any additional useful work.

[0045] Figure 6 depicts exemplary power circuit **220** for a control scheme varying a time for generating coil power according to input voltage **IV**. The following should be viewed in light of Figures 4A through 6. Pump **100** is used as an example in the discussion that follows. However, it should be understood that the control scheme described below is applicable to any pump using a solenoid coil **116** to displace an element to transfer fluid from an inlet port **104** for the pump **100** to an outlet port **106** for the pump **100** and is not limited to pump **100.** In an example embodiment, control unit **118** includes circuit **220** shown in Figure 6. Although circuit **220** is described with respect to control unit **118**, it should be understood that circuit **220** is applicable to any pump using a solenoid coil **116** to displace an element to transfer fluid from an inlet port **104**for the pump **100** to an outlet port **106** for the pump **100** and is not limited to control unit **118.**

[0046] In an example embodiment, control unit **118** includes power input line **222**, power circuit **220** includes voltage storage element **C2**, and the control unit **118** is for charging the voltage storage element with the input voltage **IV** to generate the coil power during the interval noted above for $\mathbf{T_{off}}$, and discharging the voltage storage element to supply the coil power to the solenoid coil **116.** In an example embodiment, element **C2** is a capacitor.

[0047] In an example embodiment, circuit **220** includes transistor **Q1**, for example, a metal oxide semiconductor field effect transistor (MOSFET), and timer **U1**. Timer **U1** can be any timer known in the art, for example, a 555 timer. In an example embodiment, pin **5** on the timer is clamped to establish a predetermined value against which the input voltage is compared. Pin **5** is the control voltage for a comparator circuit in the timer. In an example embodiment, a Zener diode, for example, diode **D6** is used to clamp pin **5.** To produce the values shown in Figure 5A, the voltage is clamped at 5.1V; however, it should be understood that other clamping voltage values are possible. The timer turns **Q1** off during $\mathbf{T_{on}}$ such that the coil is de-energized and **C2** is charged. The timer turns **Q1** on during $\mathbf{T_{off}}$ such that **C2** is discharged and the coil is energized.

[0048] The control scheme described above, for example, selecting the duration of $\mathbf{T_{off}}$ according to a magnitude of the input voltage **IV**, has at least the following advantages. In many applications, the magnitude of the input voltage **IV** varies according to operating conditions affecting the source of the input voltage **IV**. For example, when the pump is used in a vehicular application and a battery for a vehicle is used to supply the input voltage **IV**, the magnitude of the input voltage **IV** may be relatively lower due to the age or condition of the battery, cold weather impacting the battery, or a start-up condition for the vehicle. As a result, the magnitude of the input voltage **IV** may be undesirably low at the onset of operation of the pump and may increase as the vehicle continues to operate, for example, as the battery warms up or is charged.

[0049] Thus, during typical operation, it is expected that the input voltage **IV** will vary, for example, as shown in Figures 5A and 5B. As noted *supra*, known control schemes do not vary the duty cycle to account for such variations of the input voltage **IV.** Thus, undesirably low power is delivered to the solenoid for lower input voltage values, resulting in a loss of pumping performance, and excessive power is delivered to the solenoid for larger input voltage values, resulting in overheating of components in the pump and excessive power consumption by the pump **100.**

[0050] Advantageously, the control scheme described *supra* for Figures 5A and 6 matches generation of **CP** to actual the input voltage **IV** conditions, for example, controlling a duty cycle according to actual the input voltage **IV** conditions. As a result, **CP** is increased at lower levels for the input voltage **IV** to ensure optimal pumping rates, and **CP** is reduced at higher levels to avoid overheating components and to increase energy efficiency.

Claims

1. A solenoid pump (100), comprising:

a housing (102) with an inlet port (104) and an outlet port (106);
a first through-bore (108) connecting the inlet and outlet ports (104, 106);
a plunger (110) disposed within the first through-bore (108) and including a second through-bore (112);
a spring (114) arranged to urge the plunger (110) toward the outlet port (106);
a solenoid coil (116) arranged to displace the plunger (110) toward the inlet port (104) in response to a coil power (CP) applied to the solenoid coil (116); and,
a control unit (118) including:

an input (222) for accepting an input voltage (IV); and,
a power circuit (220) for:

generating the coil power (CP) during an interval equal to a time period (T_{off}); supplying the coil power (CP) to the solenoid coil (116); and,
selecting a duration of the time period (T_{off}) such that the duration of the time period (T_{off}) varies according to the input voltage (IV),

characterized in that,

the spring (114) is a variable rate spring with a conical shape, wherein and a first diameter (D1) of the spring 114 is less than a second diameter (D2); and
a one-way check-valve (150) is arranged at the inlet (104).

2. The solenoid pump (100) of Claim 1 wherein the control unit (118) is used for decreasing the duration of the time period (T_{off}) as a magnitude of the input voltage (IV) increases; and for increasing the duration of the time period (T_{off}) as the magnitude of the input voltage (IV) decreases.

3. The solenoid pump (100) of the Claims 1 to 2 wherein the control unit (118) is used for comparing the input voltage (IV) to a pre-determined value; and for selecting the duration of the time period (T_{off}) according to a difference between the input voltage (IV) and the pre-determined value.

4. The solenoid pump (100) of the Claims 1 to 3 wherein the control unit (118) includes a voltage storage element (C2); and the control unit (118) is used for charging the voltage storage element (C2) with the input voltage (IV) to generate the coil power (CP) during an interval; and for discharging the voltage storage (C2) element to supply the coil power (CP) to the solenoid coil (116).

5. The solenoid pump (100) of the Claims 1 to 4 wherein the control unit (118) is used for supplying the coil power (CP) at a frequency; and for selecting a magnitude of the frequency such that the magnitude of the frequency varies according to the magnitude of the input voltage (IV).

6. The solenoid pump (100) of the Claims 1 to 5 wherein the control unit (118) is used for decreasing the magnitude of the frequency as the magnitude of the input voltage (IV) decreases; and increasing the magnitude of the frequency as the magnitude of the input voltage (IV) increases.

7. The solenoid pump (100) of Claim 1 wherein the plunger (110) is arranged to fully compress the spring (114) such that coils forming the spring (114) are aligned in a direction orthogonal to a longitudinal axis (126) passing through the inlet port (104) and the outlet port (106).

8. The solenoid pump (100) of Claim 1 wherein when the coil power (CP) is not applied to the solenoid coil (116),the first diameter (D1) of the spring (114), with respect to the longitudinal axis (126), at a first end of the spring (114) closest to the inlet port (104) is less than the second diameter (D2) of the spring (114), with respect to the longitudinal axis (126), at a second end of the spring opposite the first end of the spring (114).

9. The solenoid pump (100) of Claim 1 wherein a resistance of the spring (114) to compression of the spring (114) in a direction toward the inlet port (104) increases as the spring (114) is compressed in the direction.

10. A method of operating a control unit (118) for a solenoid pump (100) including: an inlet port (104), an outlet port (106), and a first through-bore (108) connecting the inlet and outlet ports (104, 106); a plunger (110) disposed within the first through-bore (108) and including a second through-bore (112); a spring (114); a solenoid coil (116) disposed about a portion of the plunger (110); and a control unit (118), the method comprising:

urging the plunger (110) toward the outlet port (106), wherein the spring (114) is a variable rate spring with a conical shape, wherein and a first diameter (D1) of the spring 114 is less than a second diameter (D2);
accepting an input voltage (IV) at an input (222) of the control unit (118);
using a power circuit (220) of the control unit (118) to:

generate the coil power (CP) during an interval equal to a time period;
supply the coil power (CP) to the solenoid coil (116); and,
select a duration of the time period such that the duration of the time period (T_{off}) varies according to the input voltage (IV); and,

displacing, using the solenoid coil (116), the plunger (110) toward the input port (104).

11. The method of Claim 10 wherein selecting the duration of the time period (T_{off}) such that the duration of the time period (T_{off}) varies according to the input voltage (IV) includes:

decreasing the duration of the time period (T_{off}) as a magnitude of the input voltage (IV) increases; and,
increasing the duration of the time period (T_{off}) as the magnitude of the input voltage (IV) decreases.

12. The method of the Claims 10 to 11 wherein selecting the duration of the time period (T_{off}) such that the duration of the time period (T_{off}) varies according to the input voltage (IV) includes:

comparing the input voltage (IV) to a pre-determined value; and,
selecting the duration of the time period (T_{off}) according to a difference between the input voltage (IV) and the pre-determined value.

13. The method of the Claims 10 to 12 wherein supplying the coil power (CP) to the solenoid coil (116) includes:

supplying the coil power (CP) at a frequency; and,
selecting a magnitude of the frequency such that the magnitude of the frequency varies according to the magnitude of the input voltage (IV).

14. The method of Claim 13 wherein selecting the magnitude of the frequency includes:

decreasing the magnitude of the frequency as a magnitude of the input voltage (IV) decreases; and,
increasing the magnitude of the frequency as the magnitude of the input voltage (IV) increases.

15. The method of Claims 10 to 14 wherein displacing, using the solenoid coil (116), the plunger (110) toward the input port (104) includes:

fully compressing the spring (114) such that coils (116) forming the spring (114) are aligned in a direction orthogonal to a longitudinal axis (126) passing through the inlet and outlet ports (104, 106); or,
increasing a resistance of the spring (114) to compression in a direction toward the inlet port (104) as the spring (114) is compressed in the direction.

Patentansprüche

1. Solenoidpumpe (100), umfassend:

ein Gehäuse (102) mit einem Einlassanschluss (104) und einem Auslassanschluss (106);
eine erste Durchgangsbohrung (108), die den Einlass- und den Auslassanschluss (104, 106) verbindet;
einen Stößel (110), der innerhalb der ersten Durchgangsbohrung (108) angeordnet ist und eine zweite Durchgangsbohrung (112) umfasst;
eine Feder (114), die angeordnet ist, um den Stößel (110) zum Auslassanschluss (106) zu drücken;
eine Magnetspule (116), die angeordnet ist, um den Stößel (110) als Reaktion auf eine Spulenleistung (CP), die an die Magnetspule (116) angelegt wird, zum Einlassanschluss (104) zu verschieben; und
eine Steuereinheit (118), umfassend:

einen Eingang (222) zum Aufnehmen einer Eingangsspannung (IV); und
einen Leistungskreis (220) für Folgendes:

Erzeugen der Spulenleistung (CP) während eines Intervalls, welches gleich einem Zeitraum (T_{off}) ist;
Zuführen der Spulenleistung (CP) zur Magnetspule (116); und
Auswählen einer Dauer aus des Zeitraums (T_{off}), so dass die Dauer des Zeitraums (T_{off}) gemäß der Eingangsspannung (IV) variiert,

dadurch gekennzeichnet, dass
die Feder (114) eine Feder mit variabler Rate mit konischer Form ist, wobei ein erster Durchmesser (D1) der Feder (114) kleiner als ein zweiter Durchmesser (D2) ist; und
ein Einweg-Rückschlagventil (150) am Einlass (104) angeordnet ist.

2. Solenoidpumpe (100) nach Anspruch 1, wobei die Steuereinheit (118) zum Verringern der Dauer des Zeitraums (T_{off}), wenn eine Größe der Eingangsspannung (IV) zunimmt, und zum Erhöhen der Dauer des Zeitraums (T_{off}), wenn die Größe der Eingangsspannung (IV) abnimmt, verwendet wird.

3. Solenoidpumpe (100) nach einem der Ansprüche 1 bis 2, wobei die Steuereinheit (118) zum Vergleichen der Eingangsspannung (IV) mit einem vorbestimmten Wert und zum Auswählen der Dauer des Zeitraums (T_{off}) gemäß einer Differenz zwischen der Eingangsspannung (IV) und dem vorbestimmten Wert verwendet wird.

4. Solenoidpumpe (100) nach einem der Ansprüche 1 bis 3, wobei die Steuereinheit (118) ein Spannungsspeicherelement (C2) umfasst und die Steuereinheit (118) zum Aufladen des Spannungsspeicherelements (C2) mit der Eingangsspannung (IV), um die Spulenleistung (CP) während eines Intervalls zu erzeugen, und zum Entladen des Spannungsspeicherelements (C2), um die Spulenleistung (CP) der Magnetspule (116) zuzuführen, verwendet wird.

5. Solenoidpumpe (100) nach einem der Ansprüche 1 bis 4, wobei die Steuereinheit (118) zum Zuführen der Spulenleistung (CP) bei einer Frequenz und zum Auswählen einer Größe der Frequenz, so dass die Größe der Frequenz gemäß der Größe der Eingangsspannung (IV) variiert, verwendet wird.

6. Solenoidpumpe (100) nach einem der Ansprüche 1 bis 5, wobei die Steuereinheit (118) zum Verringern der Größe der Frequenz, wenn die Größe der Eingangsspannung (IV) abnimmt, und zum Erhöhen der Größe der Frequenz, wenn die Größe der Eingangsspannung (IV) zunimmt, verwendet wird.

7. Solenoidpumpe (100) nach Anspruch 1, wobei der Stößel (110) angeordnet ist, um die Feder (114) vollständig zusammenzudrücken, so dass die Spulen, die die Feder (114) bilden, in einer Richtung senkrecht zu einer Längsachse (126), die durch den Einlassanschluss (104) und den Auslassanschluss (106) verläuft, ausgerichtet sind.

8. Solenoidpumpe (100) nach Anspruch 1, wobei, wenn die Spulenleistung (CP) nicht an die Magnetspule (116) angelegt wird, der erste Durchmesser (D1) der Feder (114) in Bezug zur Längsachse (126) an einem ersten Ende der Feder (114) am nächsten zum Einlassanschluss (104) kleiner ist als der zweite Durchmesser (D2) der Feder (114) in Bezug zur Längsachse (126) an einem zweiten Ende der Feder gegenüber dem ersten Ende der Feder (114).

9. Solenoidpumpe (100) nach Anspruch 1, wobei ein Widerstand der Feder (114) zum Zusammendrücken der Feder (114) in einer Richtung zum Einlassanschluss (104) zunimmt, wenn die Feder (114) in die Richtung zusammengedrückt wird.

10. Verfahren zum Betreiben einer Steuereinheit (118) für eine Solenoidpumpe (100), umfassend: einen Einlassanschluss (104), einen Auslassanschluss (106) und eine erste Durchgangsbohrung (108), die den Einlass- und den Auslassanschluss (104, 106) verbindet; einen Stößel (110), der innerhalb der ersten Durchgangsbohrung (108) angeordnet ist und eine zweite Durchgangsbohrung (112) umfasst; eine Feder (114); eine Magnetspule (116), die um einen Abschnitt des Stößels (110) angeordnet ist; und eine Steuereinheit (118), wobei das Verfahren Folgendes umfasst:

Drücken des Stößels (110) zum Auslassanschluss (106), wobei die Feder (114) eine Feder mit variabler Rate mit einer konischen Form ist, wobei ein erster Durchmesser (D1) der Feder (114) kleiner ist als ein zweiter Durchmesser (D2);
Aufnehmen einer Eingangsspannung (IV) an einem Eingang (222) der Steuereinheit (118);
Verwenden eines Leistungskreises (220) der Steuereinheit (118) zum:

Erzeugen der Spulenleistung (CP) während eines Intervalls, das gleich einem Zeitraum ist;
Zuführen der Spulenleistung (CP) der Magnetspule (116); und
Auswählen einer Dauer des Zeitraums, so dass die Dauer des Zeitraums (T_{off}) gemäß der Eingangsspannung (IV) variiert; und
Verschieben des Stößels (110) unter Verwendung der Magnetspule (116) zum Eingangsanschluss (104).

11. Verfahren nach Anspruch 10, wobei das Auswählen der Dauer des Zeitraums (T_{off}), so dass die Dauer des Zeitraums (T_{off}) gemäß der Eingangsspannung (IV) variiert, Folgendes umfasst:

Verringern der Dauer des Zeitraums (T_{off}), wenn eine Größe der Eingangsspannung (IV) zunimmt; und
Erhöhen der Dauer des Zeitraums (T_{off}), wenn die Größe der Eingangsspannung (IV) abnimmt.

12. Verfahren nach einem der Ansprüche 10 bis 11, wobei das Auswählen der Dauer des Zeitraums (T_{off}), so dass die Dauer des Zeitraums (T_{off}) gemäß der Eingangsspannung (IV) variiert, umfasst:

Vergleichen der Eingangsspannung (IV) mit einem vorbestimmten Wert; und
Auswählen der Dauer des Zeitraums (T_{off}) gemäß einer Differenz zwischen der Eingangsspannung (IV) und dem vorbestimmten Wert.

13. Verfahren nach einem der Ansprüche 10 bis 12, wobei das Zuführen der Spulenleistung (CP) zur Magnetspule (116) umfasst:

Zuführen der Spulenleistung (CP) bei einer Frequenz; und
Auswählen einer Größe der Frequenz, so dass die Größe der Frequenz gemäß der Größe der Eingangsspannung (IV) variiert.

14. Verfahren nach Anspruch 13, wobei das Auswählen der Größe der Frequenz umfasst:

Verringern der Größe der Frequenz, wenn eine

Größe der Eingangsspannung (IV) abnimmt; und

Erhöhen der Größe der Frequenz, wenn die Größe der Eingangsspannung (IV) zunimmt.

15. Verfahren nach einem der Ansprüche 10 bis 14, wobei das Verschieben des Stößels (110) unter Verwendung der Magnetspule (116) zum Eingangsanschluss (104) umfasst:

vollständiges Zusammendrücken der Feder (114), so dass die Spulen (116), die die Feder (114) bilden, in einer Richtung senkrecht zu einer Längsachse (126), die durch den Einlass- und den Auslassanschluss (104, 106) verläuft, ausgerichtet sind; oder

Erhöhen eines Widerstands der Feder (114) zum Zusammendrücken in eine Richtung zum Einlassanschluss (104), wenn die Feder (114) in die Richtung zusammengedrückt wird.

Revendications

1. Pompe à solénoïde (100), comprenant :

un boîtier (102) avec un orifice d'admission (104) et un orifice de refoulement (106) ;

un premier alésage traversant (108) raccordant les orifices d'admission et de refoulement (104, 106) ;

un piston plongeur (110) disposé au sein du premier alésage traversant (108) et comportant un second alésage traversant (112) ;

un ressort (114) agencé pour pousser le piston plongeur (110) vers l'orifice de refoulement (106) ;

une bobine de solénoïde (116) agencée pour déplacer le piston plongeur (110) vers l'orifice d'admission (104) en réponse à une puissance de bobine (CP) appliquée à la bobine de solénoïde (116) ; et,

une unité de commande (118) comportant :

une entrée (222) pour accepter une tension d'entrée (IV) ; et,

un circuit de puissance (220) pour :

générer la puissance de bobine (CP) pendant un intervalle égal à une période de temps (T_{off}) ;

fournir la puissance de bobine (CP) à la bobine de solénoïde (116) ; et,

sélectionner une durée de la période de temps (T_{off}) de sorte que la durée de la période de temps (T_{off}) varie selon la tension d'entrée (IV),

caractérisée en ce que,

le ressort (114) est un ressort à raideur variable de forme conique, et un premier diamètre (D1) du ressort (114) est inférieur à un second diamètre (D2) ; et

un clapet anti-retour (150) est agencé au niveau de l'orifice d'admission (104).

2. Pompe à solénoïde (100) selon la revendication 1, dans laquelle l'unité de commande (118) est utilisée pour diminuer la durée de la période de temps (T_{off}) quand une grandeur de la tension d'entrée (IV) augmente ; et pour augmenter la durée de la période de temps (T_{off}) quand la grandeur de la tension d'entrée (IV) diminue.

3. Pompe à solénoïde (100) selon l'une des revendications 1 et 2, dans laquelle l'unité de commande (118) est utilisée pour comparer la tension d'entrée (IV) à une valeur prédéterminée ; et pour sélectionner la durée de la période de temps (T_{off}) selon une différence entre la tension d'entrée (IV) et la valeur prédéterminée.

4. Pompe à solénoïde (100) selon l'une des revendications 1 à 3, dans laquelle l'unité de commande (118) comporte un élément de stockage de tension (C2) ; et l'unité de commande (118) est utilisée pour charger l'élément de stockage de tension (C2) avec la tension d'entrée (IV) pour générer la puissance de bobine (CP) pendant un intervalle ; et pour décharger l'élément de stockage de tension (C2) pour fournir la puissance de bobine (CP) à la bobine de solénoïde (116).

5. Pompe à solénoïde (100) selon l'une des revendications 1 à 4, dans laquelle l'unité de commande (118) est utilisée pour fournir la puissance de bobine (CP) à une fréquence ; et pour sélectionner une grandeur de la fréquence de sorte que la grandeur de la fréquence varie selon la grandeur de la tension d'entrée (IV).

6. Pompe à solénoïde (100) selon l'une des revendications 1 à 5, dans laquelle l'unité de commande (118) est utilisée pour diminuer la grandeur de la fréquence quand la grandeur de la tension d'entrée (IV) diminue ; et pour augmenter la grandeur de la fréquence quand la grandeur de la tension d'entrée (IV) augmente.

7. Pompe à solénoïde (100) selon la revendication 1, dans laquelle le piston plongeur (110) est agencé pour comprimer totalement le ressort (114) de sorte que des bobines formant le ressort (114) soient alignées dans une direction orthogonale à un axe longitudinal (126) traversant l'orifice d'admission (104) et l'orifice de refoulement (106).

8. Pompe à solénoïde (100) selon la revendication 1, dans laquelle lorsque la puissance de bobine (CP) n'est pas appliquée à la bobine de solénoïde (116), le premier diamètre (D1) du ressort (114), par rapport à l'axe longitudinal (126), au niveau d'une première extrémité du ressort (114) la plus proche de l'orifice d'admission (104) est inférieur au second diamètre (D2) du ressort (114), par rapport à l'axe longitudinal (126), au niveau d'une seconde extrémité du ressort opposée à la première extrémité du ressort (114).

9. Pompe à solénoïde (100) selon la revendication 1, dans laquelle une résistance du ressort (114) à une compression du ressort (114) dans une direction vers l'orifice d'admission (104) augmente quand le ressort (114) est comprimé dans la direction.

10. Procédé de fonctionnement d'une unité de commande (118) pour une pompe à solénoïde (100) comportant : un orifice d'admission (104), un orifice de refoulement (106), et un premier alésage traversant (108) raccordant les orifices d'admission et de refoulement (104, 106) ; un piston plongeur (110) disposé au sein du premier alésage traversant (108) et comportant un second alésage traversant (112) ; un ressort (114) ; une bobine de solénoïde (116) disposée autour d'une portion du piston plongeur (110) ; et une unité de commande (118), le procédé comprenant :

le fait de pousser le piston plongeur (110) vers l'orifice de refoulement (106), dans lequel le ressort (114) est un ressort à raideur variable de forme conique, et un premier diamètre (D1) du ressort (114) est inférieur à un second diamètre (D2) ;
l'acceptation d'une tension d'entrée (IV) au niveau d'une entrée (222) de l'unité de commande (118) ;
l'utilisation d'un circuit de puissance (220) de l'unité de commande (118) pour :

générer la puissance de bobine (CP) pendant un intervalle égal à une période de temps ;
fournir la puissance de bobine (CP) à la bobine de solénoïde (116) ; et,
sélectionner une durée de la période de temps de sorte que la durée de la période de temps (T_{off}) varie selon la tension d'entrée (IV) ; et,

le déplacement, à l'aide de la bobine de solénoïde (116), du piston plongeur (110) vers l'orifice d'admission (104).

11. Procédé selon la revendication 10, dans lequel la sélection de la durée de la période de temps (T_{off}) de sorte que la durée de la période de temps (T_{off}) varie selon la tension d'entrée (IV) comporte :

la diminution de la durée de la période de temps (T_{off}) quand une grandeur de la tension d'entrée (IV) augmente ; et,
l'augmentation de la durée de la période de temps (T_{off}) quand la grandeur de la tension d'entrée (IV) diminue.

12. Procédé selon l'une des revendications 10 et 11, dans lequel la sélection de la durée de la période de temps (T_{off}) de sorte que la durée de la période de temps (T_{off}) varie selon la tension d'entrée (IV) comporte :

la comparaison de la tension d'entrée (IV) à une valeur prédéterminée ; et,
la sélection de la durée de la période de temps (T_{off}) selon une différence entre la tension d'entrée (IV) et la valeur prédéterminée.

13. Procédé selon l'une des revendications 10 à 12, dans lequel la fourniture de la puissance de bobine (CP) à la bobine de solénoïde (116) comporte :

la fourniture de la puissance de bobine (CP) à une fréquence ; et,
la sélection d'une grandeur de la fréquence de sorte que la grandeur de la fréquence varie selon la grandeur de la tension d'entrée (IV).

14. Procédé selon la revendication 13, dans lequel la sélection de la grandeur de la fréquence comporte :

la diminution de la grandeur de la fréquence quand une grandeur de la tension d'entrée (IV) diminue ; et,
l'augmentation de la grandeur de la fréquence quand la grandeur de la tension d'entrée (IV) augmente.

15. Procédé selon l'une des revendications 10 à 14, dans lequel le déplacement, à l'aide de la bobine de solénoïde (116), du piston plongeur (110) vers l'orifice d'admission (104) comporte :

la compression totale du ressort (114) de sorte que des bobines (116) formant le ressort (114) soient alignées dans une direction orthogonale à un axe longitudinal (126) traversant les orifices d'admission et de refoulement (104, 106) ; ou,
l'augmentation d'une résistance du ressort (114) à une compression dans une direction vers l'orifice d'admission (104) quand le ressort (114) est comprimé dans la direction.

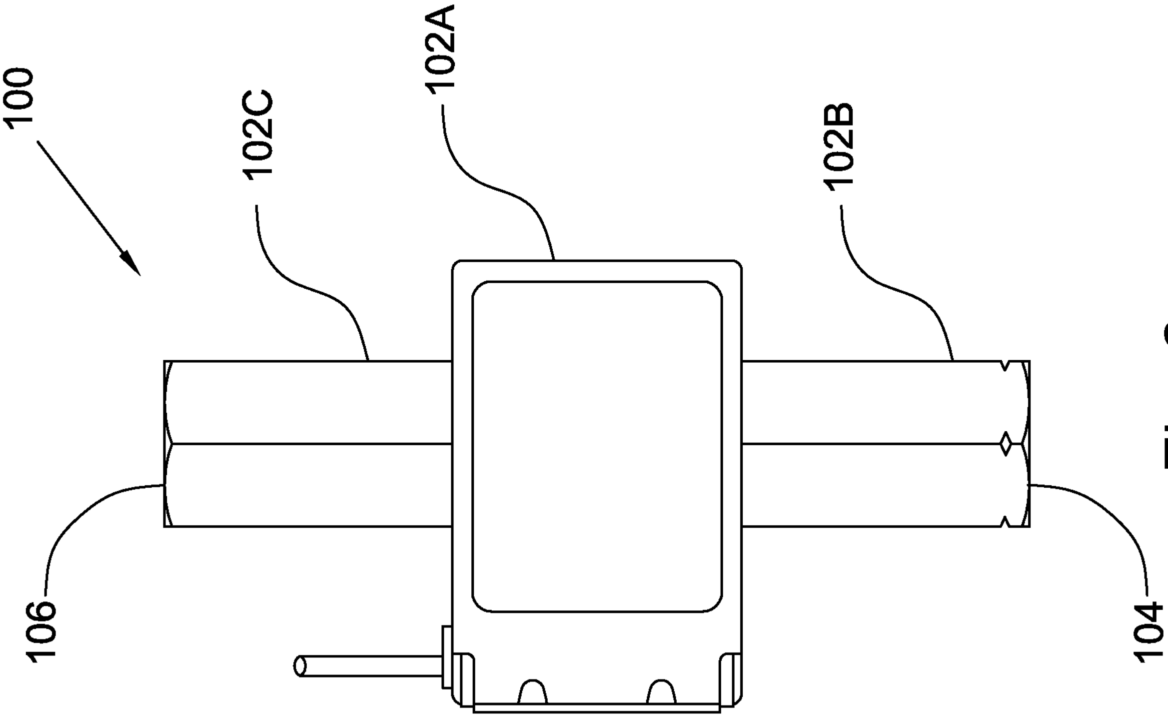
100
102C
102A
102B
106
104

Fig. 2

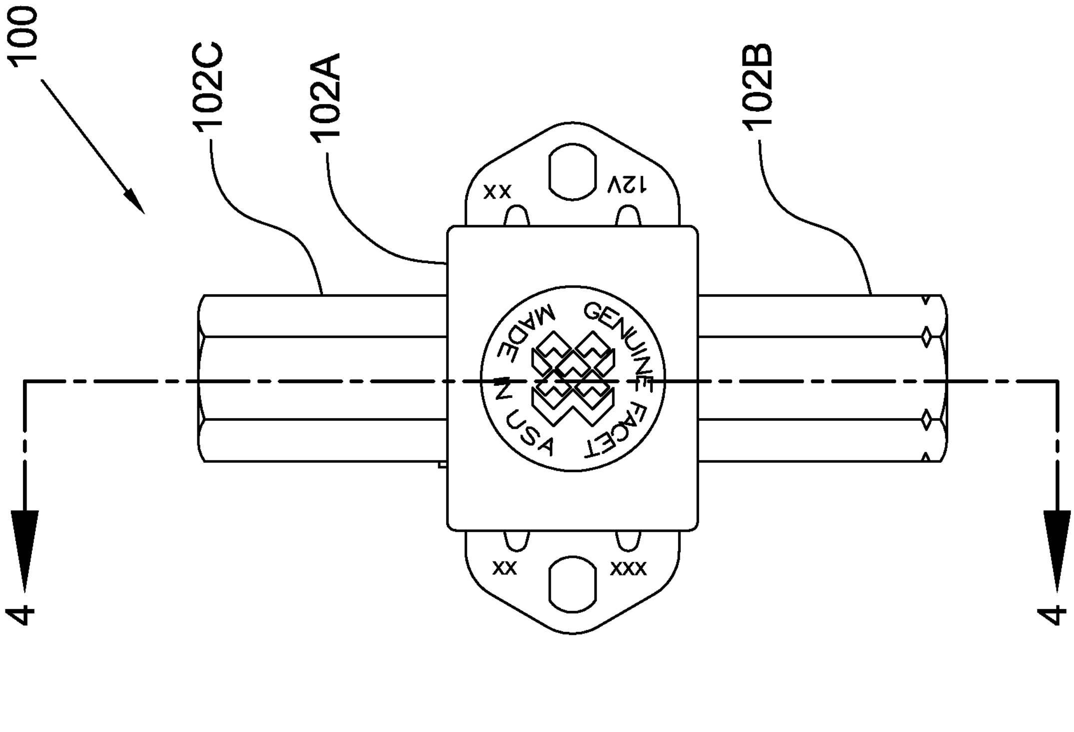
100
102C
102A
102B
xx
12V
GENUINE FACET
MADE IN USA
xx
xxx
4
4

Fig. 1

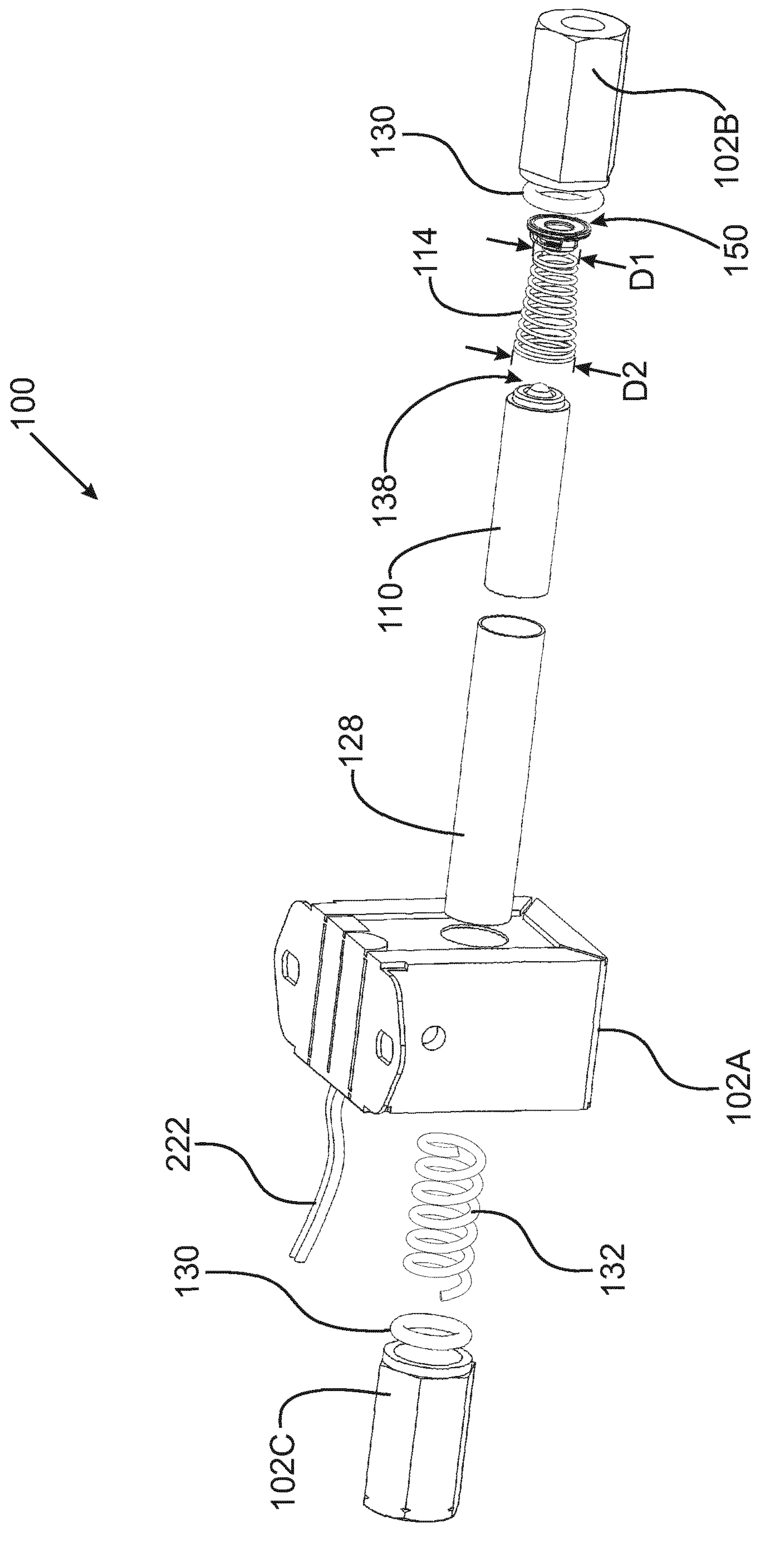

Fig. 3

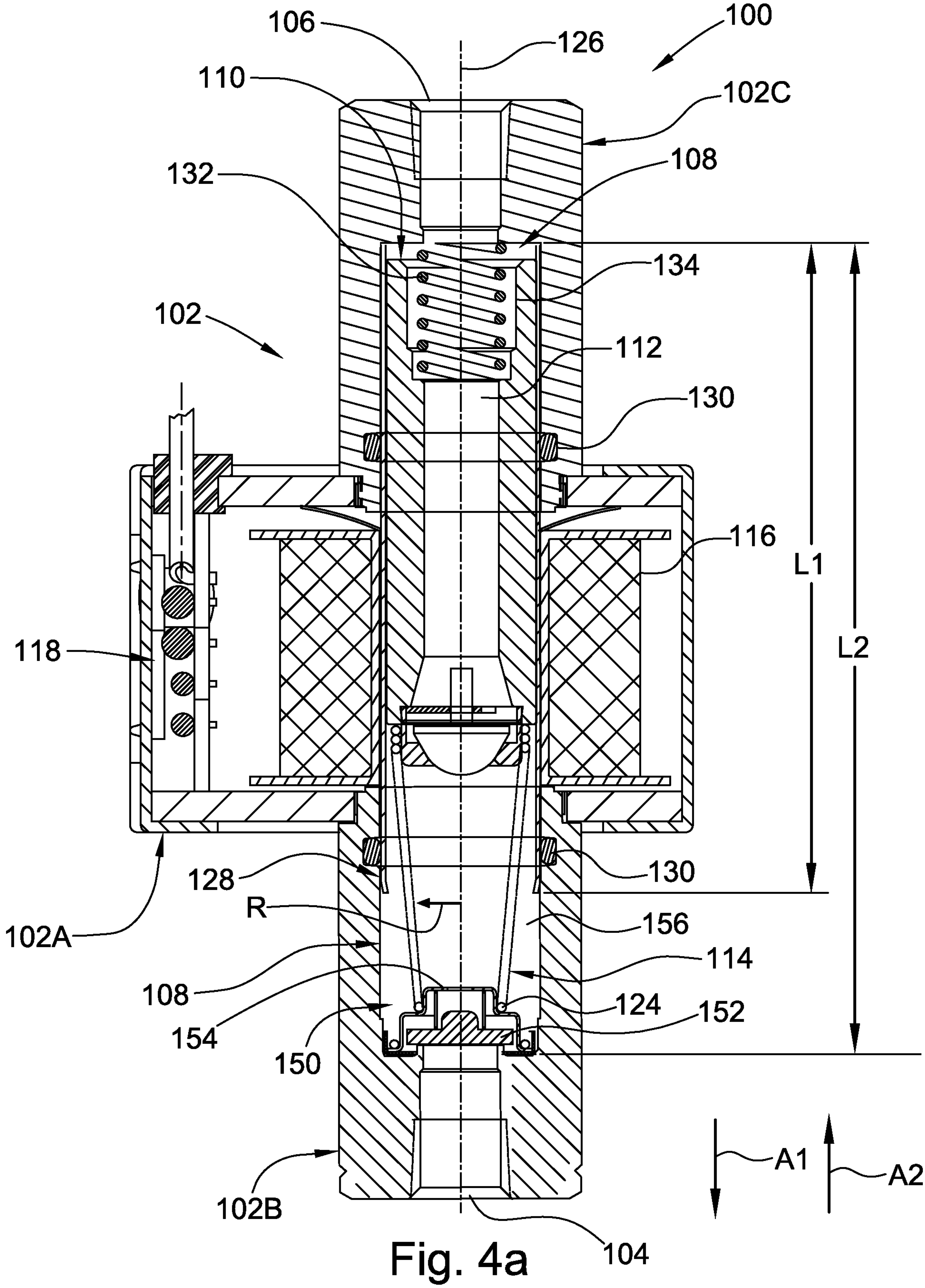
100
106
126
110
102C
132
108
134
102
112
130
116
L1
L2
118
128
130
102A
R
156
108
114
154
124
152
150
102B
A1
A2
104

Fig. 4a

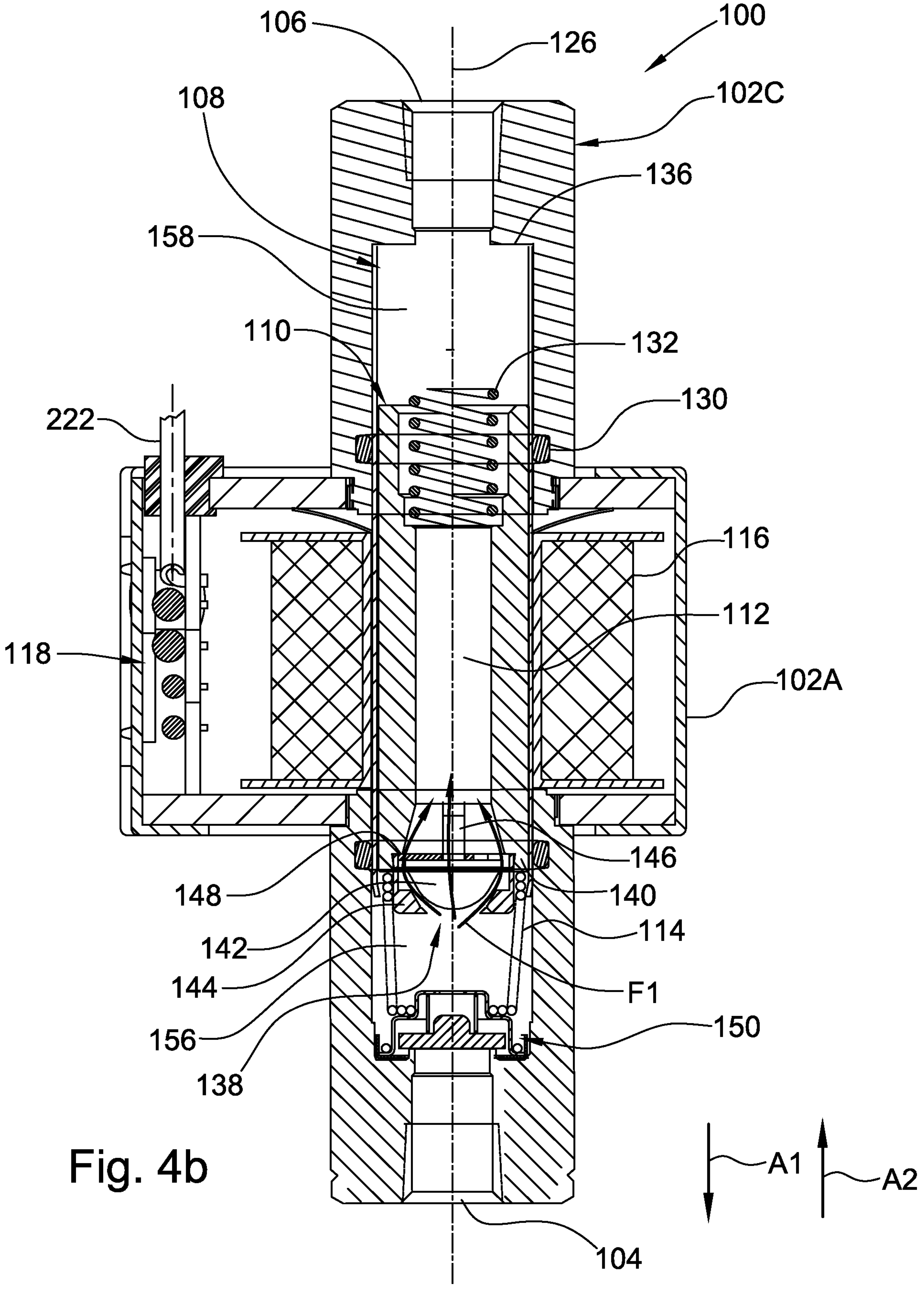
100
106
126
102C
108
136
158
110
132
130
222
116
112
118
102A
146
148
140
114
142
144
F1
156
150
138
A1
A2
104

Fig. 4b

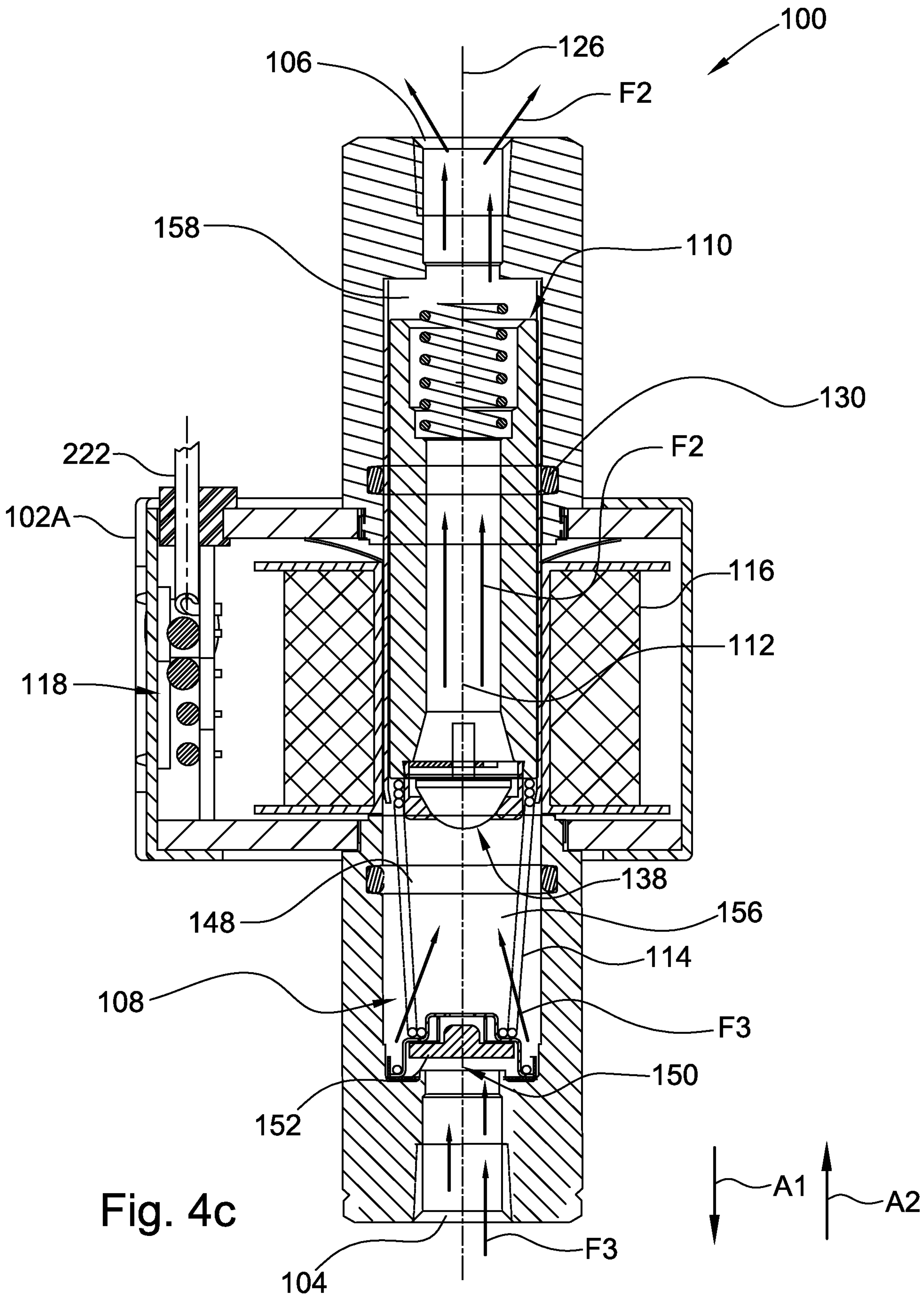
100
126
106
F2
158
110
130
222
F2
102A
116
112
118
138
148
156
114
108
F3
150
152
A1
A2
104
F3

Fig. 4c

Modified Astable Circuit							
Vdc	Toff (ms)	Ton (ms)	Duty Cycle	Frequency (Hz)	Average Current (A)	Max Current	Average Power
10.00	30.00	23.00	56.60	18.87	1.70	3.00	16.98
12.00	21.00	23.00	47.73	22.73	2.39	5.00	28.64
14.00	16.00	23.00	41.03	25.64	2.26	5.50	31.59

Fig. 5a

Astable Circuit							
Vdc	Toff (ms)	Ton (ms)	Duty Cycle	Frequency (Hz)	Average Current (A)	Max Current	Average Power
10.00	23.00	23.00	50.00	21.74	1.50	3.00	15.00
12.00	23.00	23.00	50.00	21.74	2.50	5.00	30.00
14.00	23.00	23.00	50.00	21.74	2.26	5.50	38.50

PRIOR ART

Fig. 5b

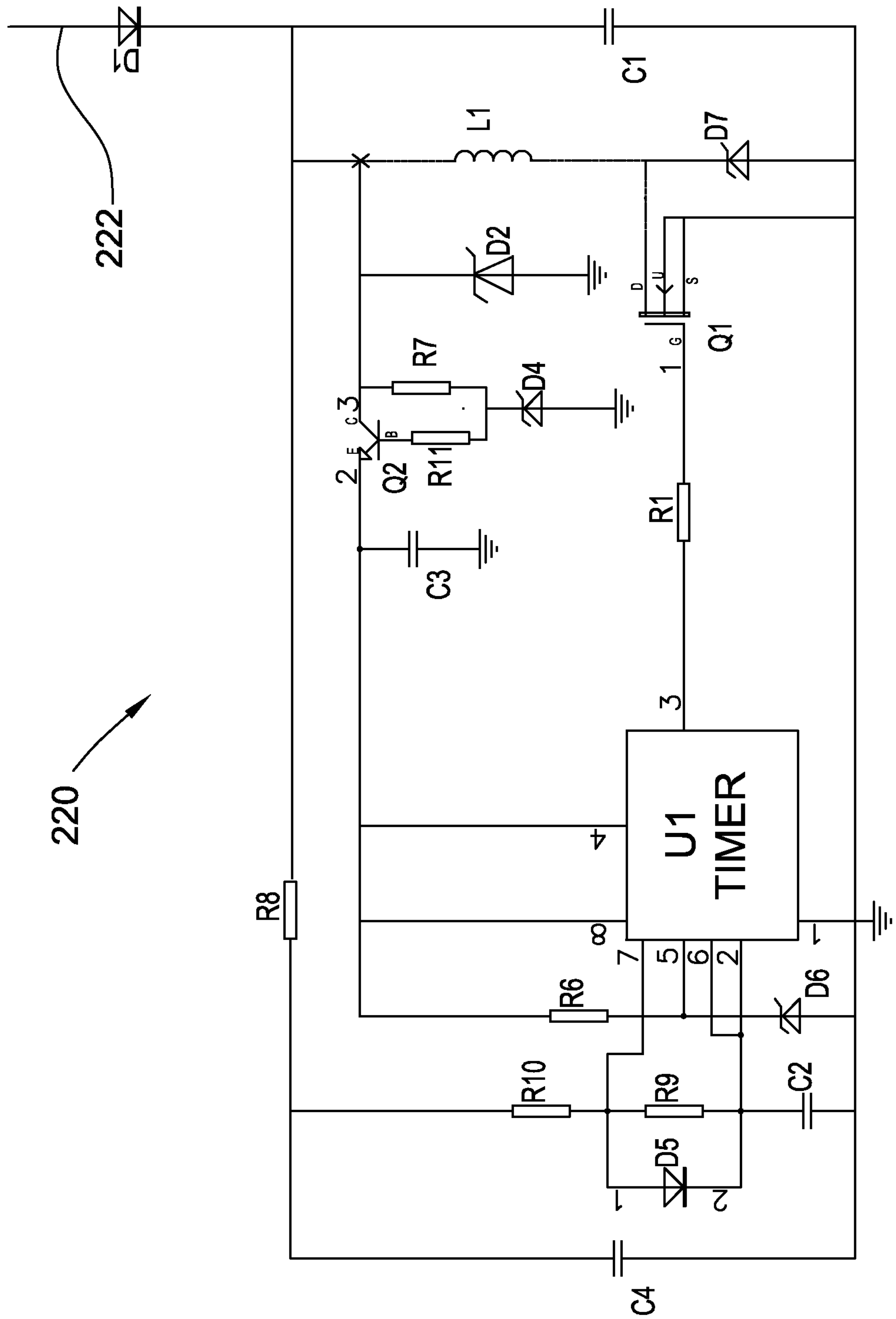
222
D1
C1
L1
D7
D2
Q1
R7
D4
Q2
R11
R1
C3
220
U1
TIMER
R8
R6
D6
R10
R9
C2
D5
C4

Fig. 6

REFERENCES CITED IN THE DESCRIPTION

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Patent documents cited in the description

- JP 2009047035 A **[0002]**
- US 4496287 A **[0003]**
- WO 03023226 A1 **[0004]**
- JP 2010065611 A **[0005]**